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54) Title: FUEL COM	POSITION			
57) Abstract There is described				
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FUEL COMPOSITION

The invention relates to a novel method of reducing the vapour pressure of fuels and to the new use of compositions.

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It is well known that liquid fuels when burned in an internal combustion engine can give rise to pollution and other undesired side effects. Furthermore, the relatively high vapour pressure of most liquid hydrocarbon fuels is known to give rise to environmental and safety problems upon storage and transportation. Numerous proposals have been advanced to reduce these side effects and enhance efficiency, eg miles per gallon. It has been realised that surfactants can play a useful role in this context but so far as we are aware none has satisfied the modern commercial criteria. It is one object of this invention to meet the need.

According to the US Environmental Protection Agency (EPA), volatile organic 15 compound (VOC) emissions from gasoline are, as ozone precursors, a major contributor to the nation's serious ground level ozone problem, which harms human health and the public welfare. In addition to automotive emissions, gasoline evaporation occurs during refining, during commercial handling, transportation, and 20 storage, and during refuelling. Because gasoline evaporation is a significant environmental problem, work was initiated at the National Alternative Fuels Laboratory (NAFL) of the University of North Dakota Energy & Environmental Research Center (EERC) to investigate evaporation rates of various gasolines and gasoline-oxygenate blends and the composition of their evaporative emissions. One 25 aspect of the work, which was funded by the US Department of Agriculture (USDA). was to compare evaporation rates and compositions of E10 evaporative emissions with those of nonethanol-blended base fuels.

Widespread commercial use of E10 fuels was originally promoted as a means to reduce gasoline consumption during the oil embargo of 1973. Current interest in ethanol as a transportation fuel involves its use as an oxygenate to reduce carbon

monoxide (CO) combustion emissions. Also, its octane-boosting quality makes it useful as a replacement for octane-supplying aromatics that are slated for removal from reformulated gasolines to be sold in ozone non-attainment areas. Despite its desirable qualities as a fuel and the fact that it is renewable, ethanol has serious competition. Ethanol supporters are locked in a long-term debate with supporters of the other major commercially available gasoline oxygenate, methyl *tertiary*-butyl ether (MTBE), over which oxygenate is best for the environment.

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A major point of contention in the debate is the approximate one-pound per square inch (psi) increase in RVP that occurs upon addition of ethanol to base fuel at a concentration of 10 vol%. However, while RVP is a useful indicator of a fuel's volatility, it is less useful as an indicator of how atmospheric interaction of vapour from the fuel (generated via evaporation or displacement during tank filling) may affect the environment in terms of ground level ozone production. Because gasolines are complex mixtures of over 200 components, the overall ozone-producing potential of a particular gasoline's vapour will depend not only on how much vapour is emitted, but also on the ozone-producing potential and concentration of each vapour component.

Surfactants have long had utility as additives which can affect the performance of fuels such as gasoline and diesel. British Patent No 2217229 describes a solubilising compound as a fuel additive. In particular there is described a composition comprising;

- 48 parts by volume of an alcohol ethoxylate:
- 3-8 parts by volume of lauric diethanolamide;
 - 3-8 parts by volume of oleic diethanolamide; and
 - 1.5-4 parts by volume of a polyglycol ether such as ethoxylated oleic acid.

Such compositions are useful as fuel additives and enable the solubilisation of water in fuels thus reducing its potential corrosive effect. However, the compositions are disadvantageous in that, *inter alia*, they require a high additive to fuel ratio.

Furthermore, they do not address the problems of emissions of gases such as CO, CO₂ and NOX, nor do they address the problems of evaporative loss due to the high vapour pressure of the fuel composition.

5 International Patent Application No WO 98/17745 describes an alternative formulation which comprises,

25% w/w of a diethanolamide,

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50% w/w of an ethoxylated alcohol, and

10 25% w/w of a fourteen carbon chain fatty acid with seven ethoxylate groups.

WO '745 especially describes fuel compositions comprising, *inter alia*, an additive made up of a fatty acid diethanolamide, an alcohol ethoxylate and an ethoxylate of a fatty acid, the degree of ethoxylation being selected so that a long term stable fuel composition is formed and, in particular, wherein, by carefully selecting the degree of ethoxylation, a balanced blend can be produced, such that the molecular weight ratios of each of the three components are substantially equivalent, for example, the molecular weight ratios are 1:1:1.

Whilst such additives provide significant reductions in emissions and are useable at low concentrations, there is still a need for a fuel composition which is capable of reducing emissions whilst maintaining performance levels.

It is known that to meet some legislation requirements fuels must have a low Reid Vapour Pressure value (RVP), e.g. under California State law, the RVP must be below 7psi.

Some modern day gasoline contains a small percentage of a condensate from natural gas pipelines. Gasoline is made up from a range of hydrocarbons, which is determined by the refining and blending processes. They may also contain minor amounts of comparatively volatile contaminants picked up during transportation, for

example, through pipe lines which have been previously used for transportation of natural gases. Pentanes are a range of C5 hydrocarbons that are typically left in the crude oil cut after the gas condensates are removed. Natural gas (methane) is extracted first from the oil field, ethane is increasingly also extracted at the well for petrochemical production of ethylene, while LPG, a mixture of C3 and C4 hydrocarbons, is liquefied under moderate pressure for use as a gas fuel. Pentane is usually the first cut off the Crude Distillation Unit at the refinery and the disposal of pentane creates a problem for the petroleum industry. Pentane has little value as a petrochemical feedstock, and blending it into the gasoline pool has the undesirable effect of raising the RVP. The aforementioned contaminants, as well as low boiling fractions arising from the refining and blending processes, all have the undesirable effect of increasing the vapour pressure of the gasoline. This undesirable effect will be further exacerbated if the fuel is blended with certain volatile oxygenating agents such as ethanol. Thus the condensate is a light fraction which is primarily pentanes although other hydrocarbons may be present. The condensate adversely affects the RVP, especially when the gasoline contains an alcohol such as ethanol.

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It is known that when gasoline and an alcohol are mixed, the resultant mixture has an increased vapour pressure. We have now surprisingly found that by adding certain surfactant compositions to a gasoline and alcohol mixture a reduction in vapour pressure (RVP) can be achieved.

Thus, according to the invention we provide a method of reducing the vapour pressure of a gasoline/alcohol mixture which comprises adding a surfactant composition comprising an alkanolamide, an alkoxylated alcohol and an alkoxylated fatty acid to a gasoline/alcohol mixture.

By the term vapour pressure we mean the Reid Vapour Pressure (RVP). Thus the method of the invention preferably reduces the RVP of the gasoline mixture to less than 8psi, preferably less than 7psi and especially between 6 and 7psi.

For the purposes of this invention the RVP is measured using the test method of ASTM D5191. Thus the vapour pressure is given as psi at 37.8°C.

It is a novel aspect of the invention to use the aforementioned surfactant composition in the reduction of RVP.

According to a further aspect of the invention we provide the use of an additive composition as hereinbefore described in the manufacture of a fuel composition having an RVP of less than 8psi.

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The alkanolamide is preferably an ethanolamide and more preferably a diethanolamide. Especially preferred are the diethanolamides and particularly the super diethanolamides. By the term super diethanolamide we mean a diethanolamide in which the nitrogen is substituted by an acyl substituent e.g. acyl C_5 to C_{20} , preferably C_8 to C_{16} , more preferably C_{10} to C_{15} . The most preferred diethanolamide has a C_{12} acyl substituent i.e. lauryl diethanolamide. Where the amides are derived from natural products this moiety will have an even number of carbon atoms, e.g. 12 for the lauryl derivative. Note, the alkyl part of this group is the R group which will be an odd number.

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There are three commercial routes to alkanolamides;

Acid + alkanolamine = alkanolamide + water

Plant or animal oil (triglyceride) + alkanolamine = alkanolamide+glycerol

Methyl ester + alkanolamine = alkanolamide + methanol

These are listed in order of increasing product quality. The route via the acid often uses an excess of alkanolamine to produce a product higher in amide than is obtainable from the acid if a stoichiometric ratio is used; these products are sometimes referred to as super amides.

The alkoxylated alcohol is preferably an ethoxylated alcohol. It is essential that the ethoxylated alcohol is an oil soluble alcohol. Therefore, alkanols are preferred and these may be primary, secondary or tertiary alkanols and especially primary alkanols. As the oil solubility of the alcohol may vary with the carbon chain length of the ethoxylated alkanol, the alkanol is preferably a C₅ to C₂₂ alkanol, more preferably C₅ to C₁₅ alkanol. The ethoxylated alcohol may comprise a mixture of alkanols. However, it is preferred that in such mixtures one alkanol will predominate. Thus, the most preferred alkanol is predominantly a C₉ to C₁₁ alkanol. In addition the degree of ethoxylation of the alcohol may be varied and the oil solubility will, generally, decrease with the increase in the degree of ethoxylation. It is preferred that the ethoxylate to alcohol ratio is greater than 2. More preferably, the ethoxylate to alcohol ratio is from between 1 and 10, preferably between 1 and 5, more preferably between 1 and 3 and especially between 2 and 3. A commercially available ethoxylated alcohol is especially preferred in which the ethoxylate to alcohol ratio is 2.75. Such an alcohol ethoxylate is available as NEODOL 91/2.5.

The fatty acid ethoxylate may comprise any conventionally known fatty acid ethoxylate. Thus the fatty acid ethoxylate may be derived from a fatty acid having from 8 to 20 carbon atoms, preferably from 10 to 18 and most preferably 14 carbon atoms (myristic acid).

The degree of ethoxylation is chosen to optimise performance in the blend with the other two selected surfactants and may be from 1 to 20, but more preferably from 5 to 12. A suitable product within this range would be, for example that derived from the addition of 7 molecules of ethylene oxide too 1 mole of myristic acid.

The values will depend on the length of the hydrophilic chain, typically an ethoxylate chain. The length of the chain will increase the extent of solubilisation because of a greater ability to solubilise.

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As with the compositions described in WO98/17745, a blend of surfactants is preferred, preferably by selecting one appropriate to the fuel, say 10 to 18 for hydrocarbon fuel, most preferably 13. In the case of an alcohol the HLB value of the surfactant is between 3 and 7, most preferably about 4. But the addition of surfactants normally create ratios of 1:1 or high volume emulsions or 5:1 ratios when the solubalisation is required at 1:100.

The invention has the ability to unify the HLB requirements of any liquid fuel which in turn allows for one dose to be used in any fuel from C5 carbon chains up. The benefit being the amount of treatment directly related to the co-solvency ability.

Preferably the ethoxylate of the fatty acid makes up about 25% by volume of the additive and further preferably the alcohol ethoxylate comprises 50% by volume of the additive.

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The surfactant additive may be added to a hydrocarbon fuel, eg diesel, petrol or alcohol, such as ethanol which may or may not be contaminated with water.

The fuel composition comprising a fuel and a fuel additive wherein the additive to fuel ratio is 0.5 - 1:1200.

The alcohol to hydrocarbon fuel ratio is from 1:8 to 1:9. Water may be present, e.g. as condensate, or added separately, in water: alcohol: fuel ratio of 0:1:8 to 0.5:;1:9 and preferably from 0.25:1:8 to 0.25:1:9.

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The additive may be present in an additive to fuel/alcohol ratio of about 0.5 - 1:1000. Preferably the additive to fuel ratio is about 1:1000, most preferably about 1:1200. In this context the fuel is the hydrocarbon fuel and alcohol mixture.

Example 1

Different blends shown in Table 1 were made and subjected to gas chromatography. The ratio of hydrocarbon: ethanol was measured by gas chromatography. The results were used to indicate the extent to which the content of the ethanol could be incorporated without exceeding an increase in the temperature at which the volatile ingredients evaporated. The results showed the amount of ethanol that could be incorporated into the hydrocarbon without increasing the temperature at which the volatile components evaporated.

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The additive comprised 60% by weight ethanolethoxylate, 20% by weight diethanolamide and 20% by weight of lauric diethanolamide. Our investigation suggests that these interact to form a blend in which the ethanolamide is a backbone.

15 Example 2

Different blends were made up and the RVP determined. The following results were obtained:

Table II

Sample	Gasoline	Ethanol	Additive	Water	RVP (1)	RVP (2)	RVP (3)
			as above				
1	90	10	-	-	7.48	7.7	7.58
2	87.5	10	2.5	· -	7.18	7.41	- 7.29
3	85.0	10	2.5	2.5	6.87	7.11	6.98
4	85.0	10	2.5	2.5	6.96	7.19	7.06

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The RVP value was measured according to ASTM D5191 and is the mean value of results calculated according to CARB (1), EPA (2) and ASTM (3) methods. In Samples 2, 3 and 4 the gasoline included a proportion of a condensate which was mainly pentanes. These results demonstrate a tendency of the additive to reduce the

RVP value, and that by selecting appropriate proportions a fuel composition can be made to meet the requirements of local legislation.

Table 1

Sample	Hydrocarbon (a)	Ethanol (b)	Pentane	Additive	Ratio (a):(b)
1	90	10	0	0	15:1
2	89	10	0	1	16.7:1
3	82	13.5	4.5	0	17.75:1
4	77.5	13.5	4.5	4.5	11.69:1

Example 3

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Various tests were conducted according to ASTM D-5191. The results are given in Tables III to IX.

Example 4

Various tests were conducted according to the 1975 US Federal City Gasoline Test.
The results are given in Tables X to XIII;

Table X:

Tests on CARB Gasoline

Table XI:

Tests on EPA

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Table XII:

Tests on Gasohol

CLAIMS

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- 1. A method of reducing the vapour pressure of a gasoline/alcohol mixture which comprises adding surfactant composition comprising an alkanolamide, an alkoxylated alcohol and an alkoxylated fatty acid to a gasoline/alcohol mixture.
- 2. A method according to Claim 1 characterised in that the RVP is less than 7psi.
- 10 3. A method according to Claim 2 characterised in that the RVP is less than 7psi.
 - 4. A surfactant composition according to Claim 3 characterised in that the RVP is between 6 and 7psi.
 - 5. A method according to Claim 1 characterised in that the alkanolamide is a diethanolamide.
- 6. A method according to Claim 5 characterised in that the nitrogen in the diethanolamide is substituted by an alkyl C₅ to C₂₀ substituent.
 - 7. A surfactant composition according to Claim 6 characterised in that the diethanolamide is a lauryl diethanolamide.
- 8. A method according to Claim 1 characterised in that the alkoxylated alcohol is an ethoxylated alcohol.
 - 9. A method according to Claim 8 characterised in that the ethoxylated alcohol is a C₅ to C₁₅ alkanol.

- 10. A method according to Claim 8 characterised in that the ethoxylated alcohol comprises a mixture of alkanols in which one alkanol predominates.
- 11. A method according to Claim 8 characterised in that the predominate alkanol is a C₉ to C₁₁ alkanol.
 - 12. A method according to Claim 8 characterised in that the ethoxylate to alcohol ratio is from between 1 and 5.
- 10 13. A method according to Claim 8 characterised in that the ethoxylated alcohol is NEODOL 91/2.5.
 - 14. A method according to Claim 1 characterised in that the fatty acid group is a C_8 to C_{20} fatty acid.

15. A method according to Claim 14 characterised in that the fatty acid group is a C_{14} fatty acid (myristic acid).

- 16. A method according to Claim 1 characterised in that the ester moiety of the 20 fatty acid ester is an alkyl ester.
 - 17. A method according to Claim 16 characterised in that the alkyl group is a C_1 to C_{10} alkyl.
- 25 18. A method according to Claim 1 characterised in that the composition comprises 25% v/v of the fatty acid ester.
 - 19. A method according to Claim 1 characterised in that the composition comprises 50% v/v of the alcohol ethoxylate.

20. A method according to claim 1 characterised in that the surfactant additive to fuel/alcohol ratio is from 0.5:1200 to 1:1000.

- 21. The use of a surfactant composition comprising an alkanolamide, an alkoxylated alcohol and an alkoxylated fatty acid ester in the manufacture of a fuel composition having an RVP of less than 8psi.
 - 22. A method of manufacturing a mixture comprising gasoline, alcohol and a surfactant composition, said surfactant composition comprising an alkanolamide, an ethoxylated alcohol and an alkoxylated fatty acid characterised in that the method comprises blending the alcohol and surfactant followed by blending with gasoline.
 - 23. A method substantially as described with reference to the accompanying examples.

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ATTN: Attn	LABORATORY 1.D: 990554-0039 DATE RECEIVED: 05/20/99 TIME RECEIVED: 16:01 REMARKS: 1-500ml amber btl	ASURE TEST METHOD DATE ASTM D-5191 (CARB) ASTM D-5191 (EPA) ASTM D-5191 (ASTM) ASTM D-5191
LABORATORY TESTS RESULTS 05/28/99	LABO DATE TIME REMA	*1 *1 0.10 PSI 0.10 PSI 0.10 PSI 0.10 PSI 0.10 PSI 0.10 PSI
LABORAT	BASE + 10% ETOH	FINAL RESULT LIN 7.16* 7.29 8.12
JOB NUMBER: 990554	CLIENT I.D	TEST DESCRIPTION REID EQUIVALENT VAPOUR PRESSURE RVP CARB CALCULATION RVP ASTM CALCULATION PRESSURE TOTAL/GRABNER INSTRUMENT

	ar btl	05/28/99
Attn	7 1.D	TEST METHOD ASTM D-5191 (CARB) ASTM D-5191 (EPA) ASTM D-5191 (ASTM) ASTM D-5191
ULTS ATTN: Attn	LABORATORY 1.D DATE RECEIVED TIME RECEIVED	PSI PSI PSI PSI PSI
LABORATORY TESTS RESULTS 05/28/99	BASE + 10% ETOH + 1% 25% NEODOL 37.5% OPE 37.5% ATLAS	
LABC	BASE	FINAL RESULT LIMITS-DILU 6.79 0.10 7.04 0.10 6.91 0.10 7.73 0.10
JOB NUMBER: 990554	CLIENT I.D	TEST DESCRIPTION REID EQUIVALENT VAPOUR PRESSURE RVP CARB CALCULATION RVP EPA CALCULATION RVP ASTM CALCULATION RESSURE TOTAL/GRABNER INSTRUMENT

	er bti	DATE 05/28/99
ttin	ED: 990554-0042 ED: 05/20/99 ED: 16:01 1-500ml amber btl	TEST METHOD ASTM D-5191 ASTM D-5191 (CARB) ASTM D-5191 (ASTM) ASTM D-5191
ULTS ATTN: Attn	LABORATORY I.D: L DATE RECEIVED: TIME RECEIVED: REMARKS:	*1 *1 *1 *1 *1 *1 *1 *1 *1 *1 *1 *1 *1 *
LABORATORY TESTS RESULTS 05/28/99	BASE + 10% ETOH + 1% AAE + 75% NEODOL + 12.5% ODE + 12.5% ATLAS	*1 0.10 0.10 0.10 0.10
LAB	90/10 REVERSE B/ + + 90/10 REVERSE + +	FINAL RESULT 6.56 6.67 7.48
JOB NUMBER: 990554	CLIENT I.D	TEST DESCRIPTION REID EQUIVALENT VAPOUR PRESSURE RVP CARB CALCULATION RVP ASTM CALCULATION PRESSURE TOTAL/GRABNER INSTRUMENT

	: 990554-0043 : 05/27/99 : 16:01 : 1-500ml amber btl	ASTM D-5191 05/28/99 ASTM D-5191 (CARB) ASTM D-5191 (EPA) ASTM D-5191 (ASTM) ASTM D-5191
ESULTS ATTN: Attn	LABORATORY I.D DATE RECEIVED TIME RECEIVED	UNITS OF MEASURE ASP PSI ASP PSI ASP PSI ASP
LABORATORY TESTS RESULTS 05/28/99		*1 0.10 0.10 0.10 0.10
LAB(90/10 (RECHECK) 90/10 (RECHECK)	FINAL RESULT 7.22 7.47 7.34 8.18
JOB NUMBER: 990554	CLIENT I.D	TEST DESCRIPTION REID EQUIVALENT VAPOUR PRESSURE RVP CARB CALCULATION RVP EPA CALCULATION RVP ASTM CALCULATION PRESSURE TOTAL/GRABNER INSTRUMENT

TABLE VIII

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	Attn	C I.D: 990554-0044 ED: 05/27/99 ED: 16:01 1-500ml anber btl	TEST METHOD ASTM D-5191 (CARB) ASTM D-5191 (EPA) ASTM D-5191 (ASTM) ASTM D-5191
SULTS	ATTN: Attn	LABORATORY I.D DATE RECEIVED TIME RECEIVED	UNITS OF MEASURE TEST METHOD ASTM D-5191 (C PSI ASTM D-5191 (E PSI ASTM D-5191 (A ASTM D-5191 (A ASTM D-5191
LABORATORY TESTS RESULTS 05/28/99			1.0 0.10 0.10 0.10 0.10
LABO		N (RECHECK) N (RECHECK)	FINAL RESULT 6.76 7.01 6.88 7.70
	JOB NUMBER: 990554	CLIENT I.D	TEST DESCRIPTION REID EQUIVALENT VAPOUR PRESSURE RVP CARB CALCULATION RVP EPA CALCULATION PRESSURE TOTAL/GRABNER INSTRUMENT

ABLE IX

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	6 ber btl	05/28/99
	: 990554-0046 : 05/27/99 : 16:01 : 1-500ml amber btl	TEST METHOD ASTM D-5191 (CARB) ASTM D-5191 (EPA) ASTM D-5191 ASTM D-5191
ATTN: Attn	LABORATORY 1.D DATE RECEIVED TIME RECEIVED	ON UNITS OF MEASURE TEST METHOD ASTM D-5191 PSI ASTM D-5191 (C. PSI ASTM D-5191 (E. PSI ASTM D-5191 (A. PS
RESULTS	LAB DAT TIME	PSI PSI PSI PSI
LABORATORY TESTS RESULTS 05/28/99	₹ ₹	*1 0.10 0.10 0.10 0.10
LABOR	EVERSE (RECHECK) EVERSE (RECHECK)	6.56 6.80 6.67 7.48
	CARBOB 90/10 REV 05/27/99 16:01 CARBOB 90/10 REV	TEST DESCRIPTION REID EQUIVALENT VAPOUR PRESSURE RVP CARB CALCULATION RVP EPA CALCULATION RVP ASTM CALCULATION PRESSURE TOTAL/GRABNER INSTRUMENT
JOB NUMBER: 996554	CLIENT I.D	TEST DESCRIPTION REID EQUIVALENT VAPOUR PRESSURE RVP CARB CALCULATION RVP ASTM CALCULATION PRESSURE TOTAL/GRABNER INSTRUME
JOB NUMB	CLIENT I.D. DATE SAMI TIME SAMP WORK DES	TEST DESCRIPTION REID EQUIVALENT VA RVP CARB CALCULAT RVP ASTM CALCULAT PRESSURE TOTAL/GR

Fuel Summary CARB Gasoline vs CARB Gasoline + AAE10 @ 1000ppm

Test No.	Vehicle	Fuel Tested FDA.75	THC	00 00	Nox (C02	CH4	NMHC	MPG
				allill/6	e e e e e e e e e e e e e e e e e e e	g/mile	g/mile	g/mile	•
5736	1993 Ford Explorer		0.151	1.697	0.239	524.16	0.027	n 1196	16 182
5736		_	0.218	2.744	0.288	485 79	0 03	0 1825	10.163
5675			0.135	1.427	0 132	582.27	25.5	0.1033	17.307
5682			0 340	000	0.100	206.37	0.021	0.110	14.586
£736			0.040	2.209	0.3/2	289.68	0.031	0.3129	28.84
2/30		_	0.073	0.772	0.148	289.58	0.008	0.0638	29.323
5/34		CARB Base, Seq#1	0.17	1.878	0.368	308.26	0.017	0.1511	27.373
-		Average	0.183	1.964	0.258	413.305	0.022	0.157	22.282
Test	Vehicle	i en	- THC	S	Š	Č	Š		
· ·			2 :	3	2	700	2 4 5	ZEZ	Z PC
ġ Z		Tested EPA-75	g/mile	g/mile	g/mile	g/mile	g/mile	g/mile	
5691	1993 Ford Explorer	CARB + AAE10, Seq#2		1.586	0.245	532.46	0.029	0 1479	15 025
5684			0.202	2.524	0.287	493.70	0.028	0 1695	17 125
5686				1.712	0.115	592 59	700	0.100	44.22
5700				3.416	0.41	287.52	0.024	0.1002	14.32
5745				705		20.102	0.030	0.2040	28.035
E7.47				00.0	0.129	794.67	0.008	0.0659	28.82
5				1.869	0.392	308.29	0.018	0.1613	27.369
		Average	0.193	1.982	0.263	418.199	0.024	0.166	22.101
		Deviation +/-	5.66%	0.89%	1.92%	1.18%	7.51%	5.70%	-0.81%

TABLE XI

Fuel Summary EPA vs EPA + AAE10 @ 1000ppm

MPG	15.682 16.893 14.103 28.328 28.318 28.318	21.648	MPG	15.808 16.848 14.123 28.235 28.146 26.729	21.648	0.00%
NMHC g/mile	0.1743 0.1947 0.1965 0.2878 0.1514	0.205	NMHC g/mile	0.1804 0.2711 0.2521 0.3268 0.1697	0.245	19.45%
CH4 g/mile	0.043 0.042 0.046 0.035 0.012	0.034	CH4 g/mile	0.048 0.046 0.056 0.034 0.014	0.037	10.16%
CO2 g/mlie	539.82 499.87 600.43 294.90 299.19 315.84	425.009	CO2 g/mile	534.78 500.54 598.06 294.89 300.57	423.663	-0.32%
Nox g/mlle	0.34 0.453 0.19 0.208 0.333	0.328	NOx g/mile	0.351 0.517 0.227 0.519 0.187	0.362	10.27%
CO g/mile	2.316 2.882 2.466 3.392 1.038 2.952	2.508	CO g/mile	2.744 3.141 3.308 3.952 1.299 3.308	2.959	17.99%
THC g/mile	0.223 0.242 0.249 0.327 0.165	0.243	THC g/mile	0.234 0.324 0.315 0.365 0.185	0.287	18.00%
Fuel Tested EPA-75	EPA Base, Seq#3	Average	Fuel Tested EPA-75	EPA + AAE10, Seq#4	Average	Deviation +/-
Vehicle	1993 Ford Explorer 1996 GMC Jimmy 1998 Dodge Ram 1991 Geo Prizm 1996 Nissan Sentra 1994 Nissan Sentra		Vehicie	1993 Ford Explorer 1996 GMC Jimmy 1998 Dodge Ram 1991 Geo Prizm 1996 Nissan Sentra 1994 Nissan Sentra	*	
Test No.	5708 5693 5692 5708 5752 5753		•	5709 5701 5702 5717 5758 5759		

TABLE X

Fuel Summary Gasohol vs Gasohol + AAE00 @ 4600ppm

				•		
MPG	16.336 17.083 14.367 29.549 28.706 27.056	22.183	MPG	16.472 17.351 14.351 29.866 28.814 26.842	22.282	0.45%
NMHC g/mile	0.1275 0.1765 0.1655 0.2309 0.1046	0.162	NMHC g/mile	0.1312 0.1938 0.1733 0.2436 0.0848	0.163	0.16%
CH4 g/mile	0.033 0.037 0.047 0.037 0.022	0.032	CH4 g/mile	0.035 0.033 0.035 0.035 0.01	0.029	-7.22%
CO2 g/mlle	519.43 495.15 589.97 283.54 295.48	415.807	CO2 g/mile	515.20 488.00 590.74 280.95 294.61 314.49	413.998	-0.44%
Nox g/mile	0.251 0.342 0.194 0.452 0.175	0.30	NOx g/mlle	0.26 0.30 0.156 0.443 0.135	0.279	-7.24%
CO g/mile	1.545 2.359 2.102 3.804 0.907 2.237	1.992	CO g/mlle	1.48 1.972 2.04 2.478 0.793 1.846	1.768	-11.25%
THC g/mile	0.165 0.219 0.273 0.118 0.194	0.198	THC g/mile	0.17 0.231 0.223 0.283 0.096	0.196	-1.25%
Fuel Tested EPA-75	Gasohol Base, Seq#5 Gasohol Base, Seq#5 Gasohol Base, Seq#5 Gasohol Base, Seq#5 Gasohol Base, Seq#5	Average	Fuel Tested EPA-75	Gasohol + AAE00, Seq#6 Gasohol + AAE00, Seq#6	Average	Deviation +/-
Vehicie	1993 Ford Explorer 1996 GMC Jimmy 1998 Dodge Ram 1991 Geo Prizm 1996 Nissan Sentra 1994 Nissan Sentra		Vehicle	1993 Ford Explorer 1996 GMC Jimmy 1998 Dodge Ram 1991 Geo Prizm 1996 Nissan Sentra 1994 Nissan Sentra		
Test No.	5722 5711 5710 5727 5764 5766	. 81	Test No.	5726 5770 5718 5735 5770 5769		



INTERNATIONAL SEARCH REPORT

In. (atlantal Application No PCT/GB 99/04155

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According to	to International Patent Classification (IPC) or to both national classifica	ation and IPC			
B. FIELDS	SEARCHED	,			
Minimum do IPC 7	ocumentation searched (classification system followed by classification ${\tt C10L}$.	on symbols)			
	tion searched other than minimum documentation to the extent that s				
Electronic d	fata base consulted during the international search (name of data bas	se and, where practical,	search terms used)	
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